Megger.

Fundamentals of partial discharge measurements

Ceren Gürbüz Electrical Engineer Power Diagnostix Systems 5 February 2020



Sebastian Dreher

Power Diagnostix Development Engineer



Send us your questions and comments during the presentation





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Fundamentals of partial discharge measurements

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Megger.



- Early research on discharge phenomena
- Occurrence of partial discharge
- Evolution of standards (Horizontal Standard IEC60270)
- Common PD detector principles
- Properties of electrical PD signals
- Conventional testing methods
- Unconventional testing methods





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- Electrical discharges, such as lightning or St. Elmo's fire, attracted researchers
- This led Benjamin Franklin to develop a lightning rod, first described in 1749
- In 1762, J. C. Wilcke invented a capacitive generator that produced electrostatic charge





- In 1777, G. C. Lichtenberg conducted the first systematic research on electrostatic discharge
- Lichtenberg built a large version of the electrophorus and found figures formed by dielectric dust on the dielectric plate
- Due to the lack of photographic options, Lichtenberg transferred the dust figures using sticky black paper



Lichtenberg nova Copy dectrica .







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- For the occurrence of partial discharge, two conditions must be met:
 - The local electric field must have reached the critical inception field ($E > E_{crit}$)
 - A free electron must be available to start the discharge avalanche
- Two main processes to derive this initial electron:
 - Ionisation by photons
 - Field emission
- The statistical properties of these processes control the appearance of the PD pattern





- *Trichel* discharge (trichel, glow, and "corona") Ionisation process: Collision ionisation
- *Streamer* discharge (filament and bunch streamer) Ionisation process: Collision and photo ionisation
- Leader discharge (stem bunch and spark) Ionisation process: Collision, photo and thermal ionisation





- Plenty of free electrons on metallic surface immediate inception of partial discharge if $E > E_{crit}$
- Polymeric low energy surfaces (PE, PP, PTFE, etc.) offer literally no free electrons — ionisation needed ????
- The sources of ambient radioactivity (cosmic photons 22 Rn, soil, fallout) cause ~2.10⁶ free electrons per second and cubic metre delayed inception
- Hence, it takes on average 15 minutes until a spherical void of 1 mm diameter is hit and discharge starts
- Common testing times of epoxy-moulded equipment often too short, e.g. dry-type transformers 3 minutes



Properties of insulation materials



- Air: 24 kV/cm bar
- Hydrogen H₂: 16 kV/cm bar
- SF₆: 88 kV/cm bar
- Transformer oil: ~150 kV/cm (20°C)
- Epoxy resin: ~300 kV/cm
- Polyethylene: >500 kV/cm (Foils up to 8000 kV/cm)
- Paschen's law: $E_{\text{Breakdown}} \sim pd (p > 1 \text{ bar})$
- Hydrogen-cooled generators: 3–7 bar
- SF₆ insulated switchgear: 3–4 bar



Wiley, 2005







No discharge although $E > E_{crit}$

- Photon provides the initial free electron
- Electric field accelerates the electron
- Discharge avalanche occurs

Charge separation after discharge

- Positive gas ions and electronics
- Space charges on the surfaces
- Residual field $E = E_{res}$

Reversed polarity during next half cycle

- De-trapping of electrons, $E > E_{crit}$
- Electric field accelerates the electron
- Discharge avalanche occurs



Visualisation of the part discharge activity

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- Historical development of representation
 - Early meter style
 - Oscilloscope, Lissajous
 - Count distribution
 - ϕ -q-n pattern
 - 3D pattern







Discharges in a spherical gas enclosure

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High availability of starting electrons

- Regular discharge for E> Ecrit
- Stable (low) discharge amplitude
- Regular partial discharge





Discharges in a spherical gas inclusion

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Low availability of starting electrons

- Random discharge event for E> Ecrit
- Higher discharge amplitude
- Typical distributed PD pattern





Discharges in a spherical gas inclusion

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High and low availability of starting electron

- Discharge pattern indicates U/U_{inc}





Discharges in a spherical gas inclusion

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Asymmetrical availability of starting electron

- Different discharge pattern per half cycle
- Positive half cycle: low availability
- Negative half cycle: higher availability





Discharges in a flat delamination

Initial process as with spherical void

- Photon provides the initial free electron
- E field accelerates the electron
- Avalanche bridges the gap

Transition into surface discharge

- Produces "Lichtenberg" figure
- Radius $r \sim E$
- "Ideal" delamination > $Q \sim E^3$

Influence of surface properties

- Different materials
- Surface conductivity
- Corrosion, ageing



Discharges in a flat delamination

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Envelope of pattern unveils discharge type

- Cavity with low electron availability $Q \sim E$
- Envelope of surface discharge type $Q \sim E^3$
- Usually, theoretical envelope only partly filled
- Ageing and corrosion increases electron availability





Treeing in polymeric material

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Asymmetrical electrode configuration

- Initial breakup of solid material (PE, PP)
- Continues as gas discharge
- Discharge increases with tree growth





Discharges at a sharp point



Asymmetrical electrode configuration

- Strongly non-symmetrical electrical field
- Low inception voltage for "Trichel" discharge
- Starts in the negative maximum
- Positive streamer: incipient break down





Discharges of floating potential

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Symmetrical pattern centred with the zero crossing

- Floating shields with small metallic gap
- Compliant in three-phase GIS (right)
- Distributed pattern with insulated gap





Influence of HV harmonics and distortion

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- Off-line transformer test: Core saturation
- Power frequency harmonics
- Load current distortion







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Revision IEC60270 —

- Diagnostix Systems COntext
 Horizontal standard: IEC 60270
 - First edition as IEC 270 in 1968
 - Second edition IEC 270 in 1981
 - Third edition IEC 60270:2000
 - Amendment IEC 60270:2015 {Ed 3.1}
 - New revision just started TC42/MT23
- Cigré documents:
 - TB662, D1.37: Guidelines for PD detection using conventional and unconventional methods
 - TB366, D1.33: Guide for PD measurements...
- IEC 62478: MEAS. of PD by el. and acoustic methods



IEC 60270:2000 — Amd1:2015

- Main points introduced
 - Recommended band width expanded
 - $\begin{array}{ll} \mbox{ Wide-band:} & 30\mbox{ kHz} \leq f_1 \leq 100\mbox{ kHz}, f_2 \leq 1\mbox{ MHz} \\ & 100\mbox{ kHz} \leq \Delta f \leq 900\mbox{ kHz} \end{array}$
 - Further calibration method "Step voltage response", Annex A.4
 - Tightened step voltage requirements $\Delta U \le 0.03 \ U_0$ during $t_d \ge 5 \ \mu s$ (steady state)
 - Test circuits for performance test of calibrators
 - Annex E showing block diagrams of PD measuring instrument principles
 - Annex H Test result evaluation with direct voltage



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• Instrument with "traditional" analogue super heterodyne principle to allow both narrow and wideband detection





• Instrument with active integration





• Instrument with early A/D conversion and digital post processing





 Instrument with "quasi-integration" at a band-pass filter and subsequent A/D conversion





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- The rise time of the electron avalanche is determined by the gaseous dielectric:
 - Under Nitrogen atmosphere, the rise time is about 1 ns and, hence, causing a bandwidth of ~350 MHz
 - Under SF_6 , an electro-negative gas, the rise time is below 200 ps and the bandwidth is up to 2000 MHz
 - Various effects reduce the signal bandwidth:
 - Dispersion, radiation and attenuation
 - Reflection and band-pass effects
 - Thus, for distributed power engineering equipment, only a reduced frequency band reaches the detector



- Modelling: cable sections of different impedance
- Reflections with each impedance change
- Corner frequency depends on the slot length





Stator winding modelling

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- Considering the wavelength: $f_c = 2.86$ MHz
- Reflection factor: Positive $(Z\uparrow)$ from core to overhang
- 80% of the signal will be reflected into the core and will not reach the coupling unit
- Measuring above f_c will strongly affect the sensitivity
- Choosing the proper measurement frequency is very important!



- Signals travelling the conductors
- Capacitive cross-coupling
- Radiation and reception
- Behaviour in freq. domain
- Behaviour in time domain









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Measuring PD

Macroscopic-physical effects Detection methods





IEC60270-compliant calibration

- PD measurements • are relative
- Charge impulse is • generated using a step voltage and an injection capacitor
- $q_0 = U_0 C_0$
- $q = q_0 \frac{C_a}{C_a + C_a}$
- $C_0 < 0.1 \text{ x } C_a$

Charge impulse calibrator connected across the test object to simulate an equivalent discharge high-voltage supply



2235/2000



- Bandwidth relation of detector, PD and calibrator signal
- The rise time of the step voltage must be short
- The resistor R_m will not cause ringing of the signal



IEC60270-compliant calibration

$$q = \int i(t) dt = \frac{1}{R_{\rm m}} \int u_{\rm m}(t) dt$$



IEC 2239/2000





IEC60270: 2015 Addendum

- - Step voltage response method
 - Rise time $t_r \le 60$ ns
 - Time to steady state ts \leq 200 ns
 - $q_0 = U_0 C_0$





Sec relies overla

pC

Pos/Net

D-K-5068-0



In practice





- Bestselling PD detector for standard Product at a glance
- measurement tasks during daily work
- User-friendly setups
- High modularity and robustness
- Frequency-selective measurements for noisy environments
- Multiplexer for multi-sample measurements
- Integrated cable fault location feature
- RIV meter optional





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Measuring PD

Macroscopic-physical effects Detection methods





- RF/VHF (1 Mhz–300 MHz):
 - RF current transformer tapping ground leads and frame connection
 - Clamp-on CTS tapping the neutral bushing

Acoustic:

- Resonant frequency of 75 kHz or 150 kHz
- Preamplifiers for acoustic sensors

Unconventional testing methods





Unconventional testing methods

- UHF coupling methods (300 Mhz–1.8
 External flange sensor
- Frequency converter unit and input protection unit
- Window sensors
 - Different sensor diameters and mounting hole configurations available for all possible GIS windows
- UHF valve sensor for transformers







ICMsystem









- Advanced state-of-the-art PD & TD measurement and analysis tool
- High-end signal pre- and post-processing
- Highest modularity and robustness
- Simultaneous real-time acquisition on up to 10 input channels
- Measurements under AC and DC
- Integrated acoustic PD location functions
- Integrated cable fault location feature
- All-in-one measurement system



- Low frequency range (IEC 60270, < 1 MHz)
 - Best coverage of the entire device under test
 - Partly hampered by noise interference
 - Best Choice for conventional off-line tests
- Medium frequency range (2–20 MHz)
 - Reasonable coverage (signal transmission)
 - Moderate noise situation
 - Best compromise for on-line monitoring (survey type)
- High frequency range (20–500 MHz)
 - Limited coverage
 - Excellent near-field detection
- Ultra-high frequency range (300–3000 MHz)
 - Reasonable coverage, acceptable number of sensors
 - Comparably low noise interference



Overview of portable products

- ICMsystem
- ICMcompact
- AlAcompact
- ICMflex
- ICMmonitor portable









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Thank you for your attention!









Survey and contact information

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Factory acceptance tests of power and distribution transformers using the ICMsystem

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Power on

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